

Non-destructive texture measurement methods for centreless X-ray diffractometers in reverse modified X (CHI) mode

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Abstract. Conventional X-ray diffraction-based pole figure measurements are realized with dedicated equipment which are accompanied with certain limitations such as sample size, geometry, and no possibility for on-site measurements. These restrictions limit the availability of texture measurements in cases when sample cutting from the object of interest is not allowed or very problematic. The present paper introduces new texture measurement method developed for mobile centreless X-ray diffractometers which are originally developed for residual stress measurements. The essence of the new method, named reverse modified X mode is that it uses the data obtained during residual stress measurement to describe anisotropic characteristics, even to the determination of pole figure. Using these methods, pole figures can be obtained with all the benefits of centreless diffractometers: no need for sample cutting, flexibility in case of large components with complex shapes, short measuring time and portability. The obtained pole figures are equivalent to the pole figures determined with conventional diffractometers. The presentation describes the measurement method and includes the validation with conventional pole figure measurements and provides instances of applications of the new technique.

1. Introduction

The definition of crystalline anisotropy, also known as texture, is key in many technological and solid-state processes since many properties such as mechanical material properties, deformation ability, magnetism, or several metallic processes such as plastic deformation, recrystallization are texture dependent. To control or to modify the texture is also crucial question during all thermomechanical treatments. The conventional techniques for texture measurement are based on neutron, X-ray or electron diffraction, and involve determining several pole figures and ODF (Orientation Distribution Function) synthesis. The general differences between these methods are the size of radiated volume and the local resolution [1-4]. Except for neutron diffraction, which is limited by source and the activation process, each method is destructive. Sample cutting is needed for conventional texture analysis by X-ray diffraction (XRD) and a very specific sample preparation technique is required for TEM (transmission electron microscopy) and electron backscatter diffraction (EBSD) investigations. The full 3D representation of crystallographic texture is given by the ODF which can be achieved through evaluation of a set of non-equivalent pole figures. Non-destructive determination of the pole figures by XRD method in many cases, such as when the test object is unique or valuable or when the sampling is forbidden by many other reasons can be beneficial [5-7]. The present paper introduces new texture measurement methods developed for mobile centreless X-ray diffractometers which are originally

Different setup of centreless diffractometer is available on the market. Such devices do not require sample cutting and virtually have no sample size limit. Those are designed to determine residual stress in a non-invasive manner even in surface mapping conditions. Mechanical stress can be represented by a stress tensor and, when applied to the material varies certain interatomic distances in the crystal. As these distances are modified along different directions in the crystal, the angle of diffraction satisfying the Bragg-condition changes. This situation results in a deformation of the diffraction cones measured by the detector. In practice, the stress on the sample may be represented by a tensor, i.e., each orientation in the crystal lattice of the sample has its own independent value for strain, and shear stress may also be present. By collecting the diffracted X-ray beam with the sample rotated at different orientations along a particular angular direction referred to as the “tilt angle” Ψ , and by comparing the deviation or shift in diffraction angle with respect to the expected diffraction angle of an unstressed sample, the stress tensor can be characterized. Tilting and rotating is generally performed by modified X or Ω modes. In contrast,

the diffraction cones are not distorted in the textured materials, but the intensity distribution on the cone surface will be different. In practice, this texture is often represented using a pole figure, in which a specified crystallographic axis (or pole) from each of a representative number of crystallites is plotted through stereographic projection, along with directions relevant to the processing history of materials. During the determination of stereographic projection tilting and rotating of the sample is performed, conventional pole figure measurements are carried out in X mode.

During operating the centreless diffractometer in contrast to conventional one the measured object is stationary while the diffractometer is tilted around the object. However, the main difference in stress and conventional texture measurement is not the tilting of the sample but the beam path. Therefore, the transition between the two methods (stress and texture test) is not obvious. While describing the solution of transition, axes, angles, directions regarding the centreless diffractometer system are distinguished by apostrophe (') from the conventional ones. There are basically two ways to find the solution. First case is when the coordinate (φ rotating and χ tilting angles) of the conventional pole figure is fixed and used to calculate the appropriate φ' rotating and χ' tilting angles to be applied on the centreless diffractometer. This modified X method is described in detail in a previous article [9]. The other case is a much more convenient solution for the user, when the pole figure coordinates of the applied rotating and tilting angles of the centreless diffractometer (φ' , χ') are calculated. This is the reverse modified X method and is described in this manuscript. The advantage of this method is that in this case stress values can also be determined from the measurement data, which in many cases can also provide useful information. To make the difference between the modified X mode and the reverse modified X mode easier to understand, we will use the same graphics and nomenclature. Figure 2 shows the beam path and the different set ups. The main parts of the conventional and the centreless diffractometer setup are indicated: C-collimator, A, B detectors, S_0 , S_0' incident beam, S_A , S_B , S_A' , S_B' diffracted beams, m_A , m_B , m_A' , m_B' -measurement directions or diffraction vector or normal of the plains in Bragg position.

2.3. Reverse modified X mode

It is possible to assign not only a predetermined χ_i value to a specific tilting value, but to determine the pole figure coordinates from the data obtained during the intended use of the equipment (eg. residual stress measurement), if the position of the sample (β - angle between the Ω and Ω' or the physical rotation of the centreless diffractometer around the Φ' axis) and the value of the tilting (χ') taken during the measurement and the Bragg-angle (2θ) value are known. The transition from the centreless system to the conventional one is not obvious, because of the different beam passes of the two systems. The pass of the measuring direction vector is represented by concentric cones series during operation in both systems. For simplicity, let us consider the length of the cone generatrix unity. The two rotating axes of the two cones series are perpendicular to each other (Figure 3.). Determination of the coordinates of the intersections (P at $\chi'=0$ and Q at $\chi'\neq 0^\circ$.) is the crucial point when measuring pole figures with centreless diffractometers. The questions are the φ and χ value at these positions. Equations 1-11 give the solution. Notice that the R_i value is difference between the modified X and the reverse modified X mode.

Since $2\psi'$ is the complementary angle of $2\theta'$ (Figure 2.), thus, ψ' can be calculated from the Bragg-angle ($2\theta'$) by (1) [9].

$$\psi' = (180 - 2\theta)/2 \quad (1)$$

M' is the perpendicular projection of m_B' on the tilting axis (X) and can be calculated according to (2) and Figure 3 [9].

$$M' = \sin \psi' \quad (2)$$

U' is the distance of P or Q from the X and can be calculated according to (3) [9].

$$U' = \cos \psi' \quad (3)$$

L_i is the distance of the vertical projection of P or Q from X and can be calculated by (4) [9].

$$L_i = \sin \chi'_i * \cos \psi \quad (4)$$

R_i , the perpendicular projection of m_B' on the sample surface can be calculated according to (5).

$$R_i = \sqrt{M'^2 + L_i'^2} = \sqrt{(\sin \psi)^2 + (\sin \chi'_i \cos \psi)^2} \quad (5)$$

α is the angle between R and Ω axis and can be calculated according to (6).

$$\alpha_i = \arcsin\left(\frac{M'}{R_i}\right) = \arcsin\left(\frac{\sin \psi'}{\sqrt{(\sin \psi')^2 + (\sin \chi'_i \cos \psi')^2}}\right) \quad (5)$$

χ_i can be calculated using equation (7).

$$\chi_i = \arcsin(R_i) = \arcsin\left(\sqrt{(\sin \psi')^2 + (\sin \chi'_i \cos \psi')^2}\right) \quad (6)$$

Then, φ_j can be calculated according to equations (8), (9), (10) and (11) within the I., II., III. and IV. quarter of the current coordinate system, respectively (Figure 3.), where β is the angle between Ω and Ω' or the physical rotation of the centreless diffractometer around Φ' axis [9].

$$\varphi_j = \alpha_i + \beta_j \quad (7)$$

$$\varphi_j = (180 - \alpha_i) + \beta_j \quad (8)$$

$$\varphi_j = (180 + \alpha_i) + \beta_j \quad (9)$$

$$\varphi_j = (360 - \alpha_i) + \beta_j \quad (10)$$

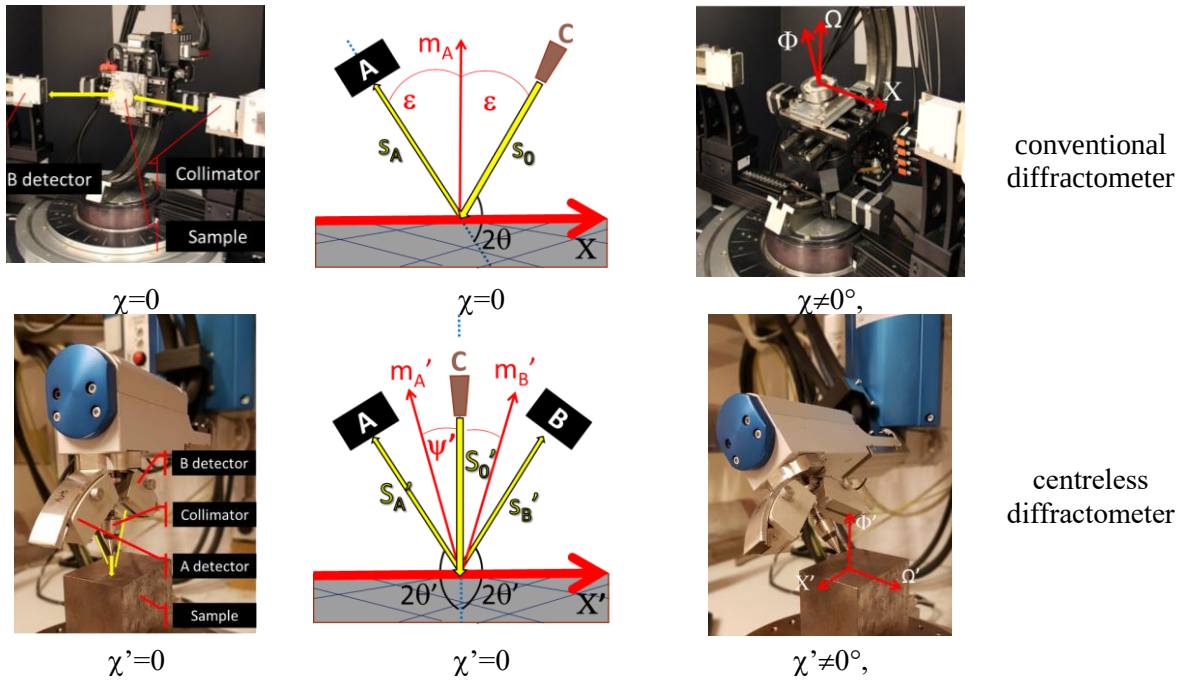


Figure 2. Beam path of different diffractometer configurations at $\chi \neq 0^\circ$, and $\chi = 0^\circ$. [9]

After absorption (defocusing) correction, the measured intensity values are available as a function of χ and φ , from which the pole figure can be constructed.

3. Results and the validation of the new method

A 3104 type cold rolled aluminium sheets were chosen for the validation. Figure 4 shows the $\{222\}$ pole figures determined by a conventional and the centreless diffractometers. The cold rollings were performed by a Von Roll experimental rolling mill, having 220 mm roll diameter, using 50 m/min rolling speed and mineral oil based liquid lubricant. The sheets were cold rolled from 4.8 mm thickness to 1 mm (H20K) and from 4.8 to 0.2 mm (H10K), respectively. Conventional pole figure measurements were carried out by Bruker D8 Advance diffractometer equipped Eulerian cradle and Co $K\alpha$ radiation source

operating with 40kV tube voltage and 40 mA tube current. Pole figure were measured up to 75% tilting with 5° increments and visualised by the TexEval software. The new method was introduced using a Stresstech XStress 3000 G3R type centreless diffractometer with CrK α source operating with 30 kV tube voltage and 8 mA tube current. The used χ' values were -59°+59°, with 5° increments, β was chosen as -90°...+90°, with 5° increments. The absorption corrected pole figures were visualised by Origin software. For both equipment, absorption correction was performed on Al powder. It is evident that the relevant information of the pole figures of the two methods is the same.

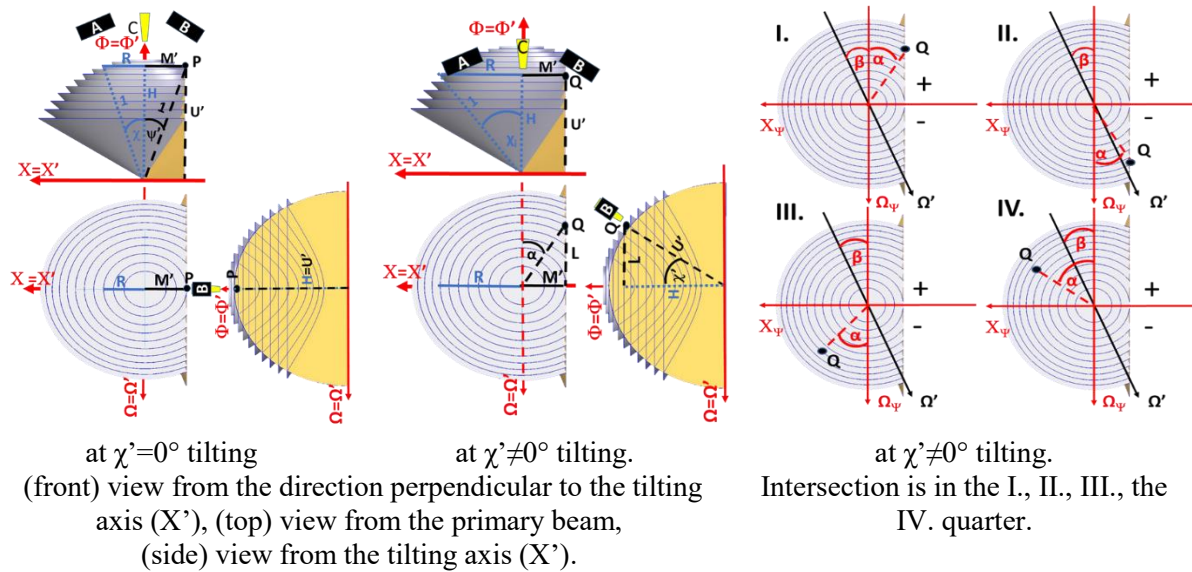


Figure 3. Theoretical view of measurement directions of different configuration X and X' modes. Q and P are the intersections. Interpretation of parameters. [9]

4. Summary

The reverse modified X mode as a new non-invasive pole figure measurement method was introduced based on the non-destructive residual stress measurement performed with centreless diffractometer. The centreless diffractometers generally operate by modified X (CHI) and Ω (OMEGA) modes. The full method to use modified X mode for pole figure determination had already shown [9]. In this paper the mathematical background demonstrated for the reverse modified X mode. It means that the centreless diffractometer operates as during residual stress measurements and the mathematical correlations describing the connection of the data set from the residual stress measurement with the coordinates of the pole figure have been shown. Each of the two measurement methods can be implemented in any case where the sample cut is not allowed, the surface is not even flat and the object to be examined is too large. The limit of the methods is that the centreless diffractometers operate at high value of 2θ diffraction angles based on the principle of residual stress measurements so that these pole figures can be detected. The lack of the method can be eliminated by a diffractometer system attached to the robot arm (X mode).

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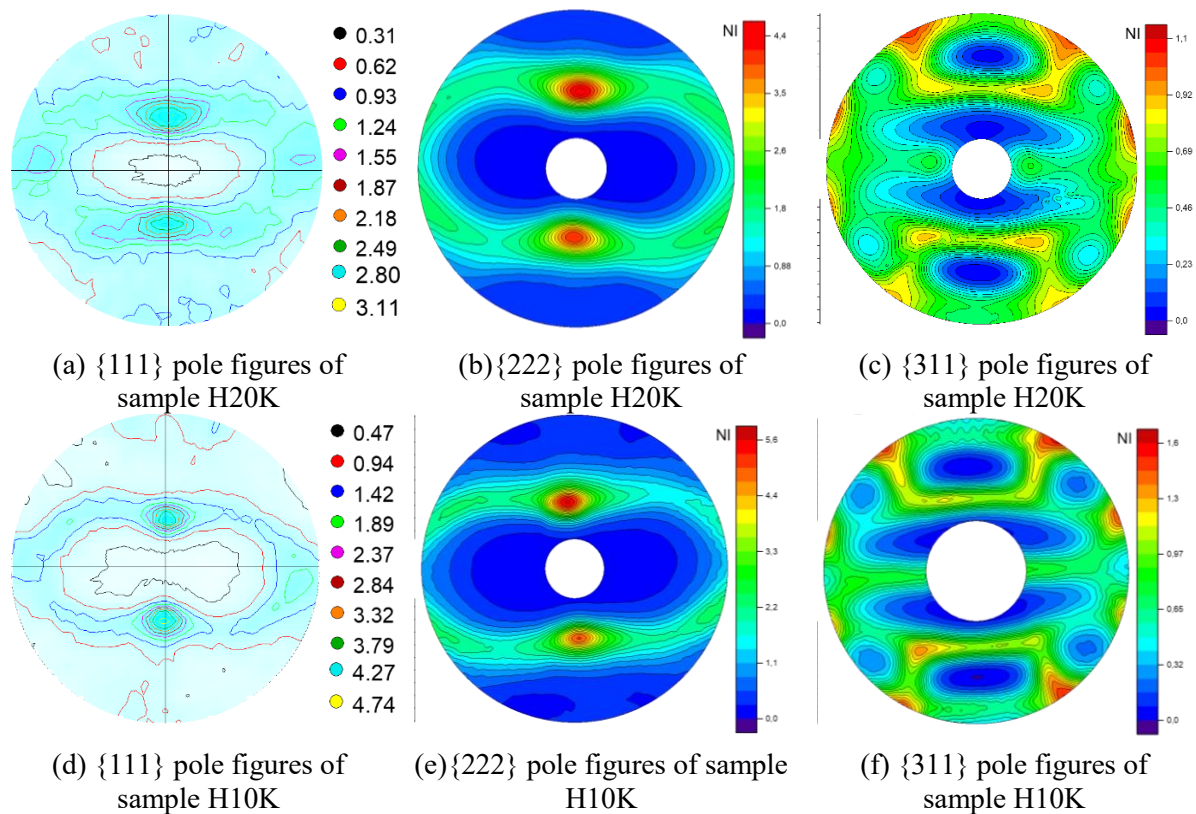


Figure 3. Pole figures and pole density numbers of cold rolled 3104 type aluminium sheets after different cold rollings. (a, d) pole figures measured with a conventional diffractometer (max $\chi=75^\circ$); (b,c,e,f) pole figures measured with a centreless diffractometer (max $\chi'=60^\circ$) in reverse modified X mode

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